Design and Analysis of Structural Members of the Jib Crane

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Abstract:- This study has been undertaken to investigate and estimate design needs and propose optimum solution for lifting facility, and detailed calculation for lifting facility at Water Treatment Plant. Prior to decide optimum solution for the problem, evaluation of design concept has been done through various steps. Function decomposition and identification of individual function of the each subsystem, internal and external search for creating solution domain, next, best optimum solution has been selected via logical approach which was pairwise comparison and weighted decision matrix, and detailed calculation is performed as final step of the research.

Keywords:- Jib Crane, Payload, Tensile Strength, BS Standards.

I. INTRODUCTION

Lifting facility availability is essential for the routine and breakdown maintenance work at pumps station, without having proper lifting facility; stakeholders face difficulties, consequently, safety issues also shall be raised during the maintenance work. Boom and mast are the major structural members of the jib crane, with this study; detailed calculation is conducted for performing proof-of-competence determinations of the steel structures of cranes in term of material selection, requirements, methods, and parameter values. [1]

II. KEY TECHNICAL FEATURES OF THE JIB CRANE

Lifting and Lowering Movement of Payload

Lifting, lowering of the load should be electric powered hoist unit that can handle maximum load approximately 1.5 Ton and maximum lifting height is 7m.

> Trasverse Movement of Payload

Transverse movement approximately 15m distance along one axis with bi-directional movement by considering area where lifting facility should access.

III. METHODOLOGY

Extracted deign parameters for the jib crane and loads acting on the structural members were evaluated, next, possible load combinations also estimated to obtain maximum loads and bending moments. Then, critical section of the boom and mast was determined, design stresses have been calculated accordingly, buckling and verticality of the mast has also been considered. Finally welded and bolt joint competence calculation was performed while power requirement for hoisting and travelling were also calculated.

IV. MATERIAL, METHOD AND CALCULATION

Design parameters as indicated in table I, when selected the structural members, following parameters have been taken into consideration.

Table 1 Design Parameters		
Maximum Lifting Height	H_L	7 <i>m</i>
Jib Crane Total Column Height	H_c	3 <i>m</i>
Jib Crane Boom Length	H _s	3.1 <i>m</i>
Slewing Angle	α_{Slew}	180°

Section of mast and boom

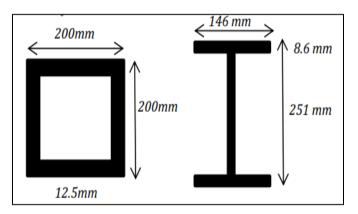


Table 2 Specification of	of the Mast
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Mass per meter	72.3 kg/m
Area of section (A)	92.1 cm ²
Second moment of inertia (I)	5340 <i>cm</i> ^₄
Height of the mast	4.25 <i>m</i>
Base plate size	600×600
Material	S275

Table 3 Sp	ecification	of the l	Boom
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Mass per meter	31.1 kg/m
Area of section (A)	39.7 cm ²
moment of inertia(I)-Y-Y axis(2 nd)	4410 <i>cm</i> ⁴
Length of the mast	3.1 <i>m</i>
Material	S275

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Dead weight, unrestrained grounded load, sudden release of the loads, tilted loads were taken into account for the jib crane according to the *ISO* 8686-1:2012 E [2], and calculated load combination using limit state method, maximum forces acting along X, Y and Z direction of the coordinate system were 0.855kN. 0.855kN and 17.78kN respectively as indicated in the Figure 1,

Analysis of Structural Member-Boom

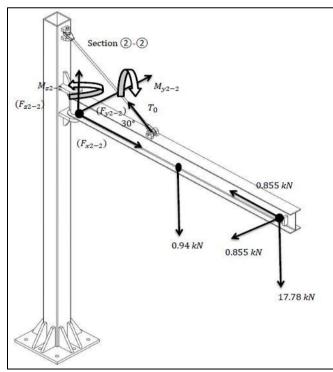


Fig 1 Free Body Diagram of Section 2 of the Boom

Free body diagram of the boom expressed possible force and moments acting on the boom, all forces acting along X, Y, and Z obtained from equation of equilibrium, bending moments were calculated accordingly.

Bending moment around x, y and z axis,

 $M_{x2-2}, M_{y2-2} = 0, M_{z2-2} = 2.65 \, kNm \tag{1}$

Normal stress calculated as follows

$$\sigma = \frac{P}{4} = 24.899 \, MPa \tag{2}$$

Maximum normal stress due to M_{z2-2} ;

$$\sigma_{z-max} = \frac{M_{z_{z-2}}C_y}{l_z} = 4.32 \, MPa \tag{3}$$

By inspection the normal stress at section (2-2);

 $\sigma_{\max(2)-(2)} = 29.219 \, MPa$ (4)

Calculating shear stress at section (2)-(2);

$$\tau_{2-2} = \frac{VQ}{It}, \tau_{2-2} = 27.7 \, MPa \tag{5}$$

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Proof for structural, boom according to the BS ISO 20332:2016 [3]

$$\sigma_{\max(2)-(2)} \leq$$
 Tensile stress of the material (6)

$$\tau_{\max(2)-(2)} \leq$$
 Shear stress of the material (7)

Deflection of the boom was calculated to check whether boom is in order to accept the structural member according to standards;

$$\delta_{B1} = \frac{qL^4}{8EI}, \delta_{B1} = 0.07 \, mm \tag{8}$$

At the end of beam, maximum deflection due to weight of the load and hoist;

$$\delta_{B2} = \frac{FL^3}{3EI}, \delta_{B2} = 2.45 \, mm \tag{9}$$

The maximum deflection of the beam produced by the dead weight and weight of the trolley and rated load shall not exceed 1/600 of the span of the crane as per the *IS* 807-2006 [4], therefore, deflection limit is satisfied.

Analysis of Structural Member-Mast

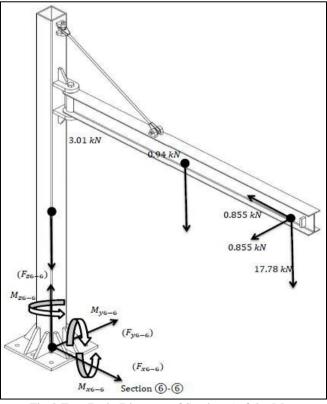


Fig 2 Free Body Diagram of Section 6 of the Mast

For the mast, forces and bending moments were calculated using free body diagram, possible highest compressive stress and shear stress were calculated using equation (1), (2), (3) and (5) proof calculation performed as per the condition (6) and (7) to verify competence of the structural member.

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Following design parameters have been calculated and listed below.

Table 4 Calculated Parameters for Mast	
Parameter	Value
$(F_{x6-6}), (F_{y6-6}), (F_{z6-6})$	0.86 kN, 0.86 kN, 21.73 kN
$M_{x6-6}, M_{y6-6}, M_{z6-6}$	2.565 kNm, 52.55 kNm, 0 kNm
σ , σ_{x-max} , σ_{y-max}	2.36 MPa, 4.8 MPa, 98.4 MPa
$\sigma_{\max(6)-6}$	105.56 MPa
$ au_{\max(6)-(6)}$	0.3 <i>MPa</i>

Buckling of the mast, proof of stability calculation was performed to verify stability of the structural member in order to withstand the rated load.

Critical buckling load of the mast and slenderness are calculated by the equation (11), (12), as in [3, Table 12.];

$$N_k = \frac{\pi^2 EI}{4L^2} \tag{10}$$

Calculated value for the critical buckling load and slenderness of the mast are 1533.1 *kN* and 1.26 respectively.

Limit design compressive force, as in [3, eq. 47, eq. 46];

$$\lambda = \sqrt{\frac{f_y A}{N_k}} \tag{11}$$

$$N_{Rd} = \frac{K f_y A}{\gamma_m} \tag{12}$$

Calculated limit design compressive force as per equation (12) equal to 1082 kN.

Proof for elastic stability, following condition shall be satisfied according to *BS ISO 20332:2016*[3];

$$N_{Rd} \le \frac{N_k}{1.2 \,\gamma_m} \tag{13}$$

 $1082 \ kN \le 1161.44 \ kN \tag{14}$

Therefore, mast elastic stability is satisfied as per *BS ISO* 20332:2016.

Evaluating verticality of the mast due to buckling and horizontal loads, secant formula, as in [5, eq. 13-16];

$$v_{max} = e \left[sec \left(\sqrt{\frac{P}{El} \frac{L}{2}} \right) - 1 \right]$$
(15)

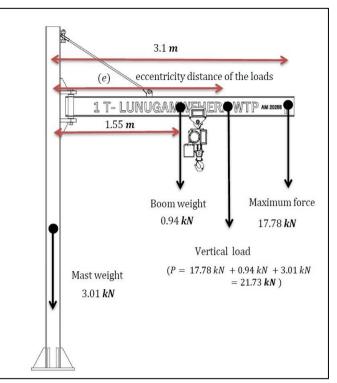


Fig 3 Diagram of Eccentric Loading to the Mast and the Boom

Calculating eccentricity of the load;

$$e = \frac{17.78 \text{ kN} \times 3.1 \text{ m} + 0.94 \text{ kN} \times 1.55 \text{ m} + 3.01 \text{ kN} \times 0 \text{ m}}{17.78 \text{ kN} + 0.94 \text{ kN} + 3.01 \text{ kN}} = 2.6 \text{ m}$$
(16)

Using equation (15),

$$v_{max} = 2.5 mm \tag{17}$$

Maximum deflection of the mast due to horizontal force acting on the mast can be calculated by the using following formula;

Total maximum deflection of the mast, using (17), (18);

$$\delta_{max} = \frac{PL^3}{3EI} = 0.7 mm \tag{18}$$

$$(v_{\max}) + \delta_{max} = 3.2 \, mm \tag{19}$$

The maximum deflection of the column produced by the horizontal and vertical load shall not exceed 1/600 of the span of the crane as per the *IS* 807-2006.

$$(v_{\max}) + \delta_{max} \leq Limit \ Design \ Value$$
 (20)

Therefore, deflection limit is satisfied.

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V. CONCLUSION

Structural members, boom and mast have been subjected to essential analysis according to its behavior; payload and its predictive and un-predictive actions have also been considered to the load calculation. Considering all of them, boom and mast were analyzed capabilities to withstand under pre described conditions.

It was concluded, with supporting rope arrangement; boom sectional dimensions can be taken to optimum level using supporting rope wire rather than using large heavy sections for the said structural member.

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